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Introduction

3G wireless communication

- ✓ Time resource: 2 MHz bandwidth at 1 GHz carrier frequency
- ✓ Spectral efficiency : 1 bps/Hz, Capacity: 2 Mbps

4G wireless communication

- ✓ Time resource: 20 MHz bandwidth at 2 GHz carrier frequency
- ✓ Space resource (MIMO): number of antennas = 4
- ✓ Spectral efficiency : 15 bps/Hz, Capacity: 300 Mbps

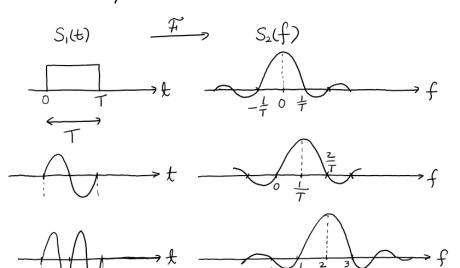
5G wireless communication

- ✓ Time resource: 1 GHz bandwidth at 28 GHz carrier frequency.
- ✓ Space resource: number of beams * polarization
- ✓ Spectral efficiency: 20 bps/Hz, Capacity: 20 Gbps

Introduction

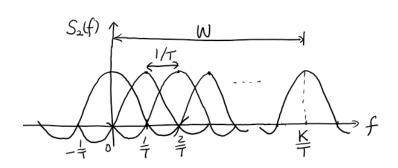
- Number of information from time and frequency resource
 - \checkmark Time resource: T, frequency resource: W
 - ✓ Time and frequency have fourier transform relationship.
 - ✓ Number of sinc functions in frequency domain

$$K = \frac{W}{1/T} = WT$$
 (Number of information)



$$S_2(f) = \int_{-\infty}^{\infty} S_1(t) e^{-j2\pi f t} dt$$

$$S_1(t) = \int_{-\infty}^{\infty} S_2(f) e^{j2\pi f t} df$$

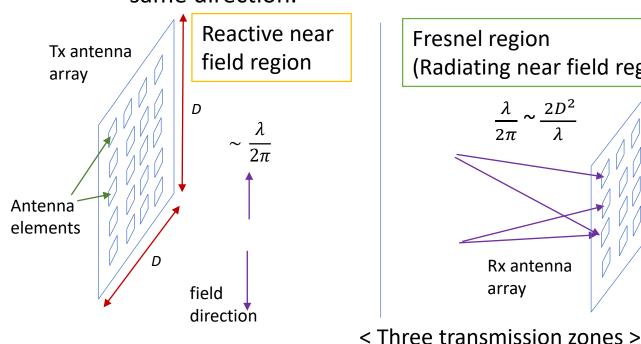


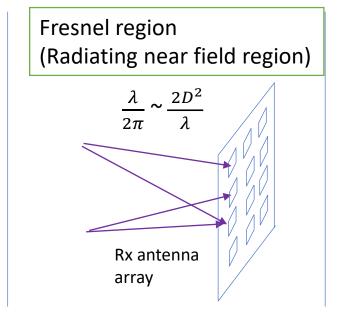
< Utilization of time and frequency resources >

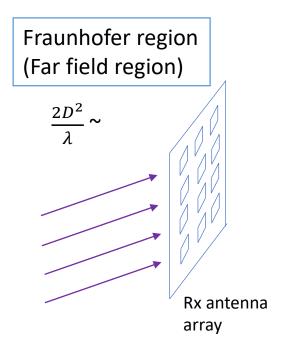
1 Introduction

- 6G capacity requirement
 - ✓ The goal of 6G: 1 Tbps capacity
- 6G frequency resource and capacity
 - ✓ Sub-THz band: 100 GHz~300 GHz
 - ✓ Available bandwidth: 5 GHz~10 GHz
 - ✓ Required spectral efficiency: 100~200 bps/Hz
 - √ (64QAM) * (polarization) = (6 bps/Hz) * 2 = 12 bps/Hz
- Can we achieve the spectral efficiency of 100~200 bps/Hz for 6G 1 Tbps capacity?
 - ✓ Yes, capacity can be increased by utilizing spatial resources in the Fresnel region.

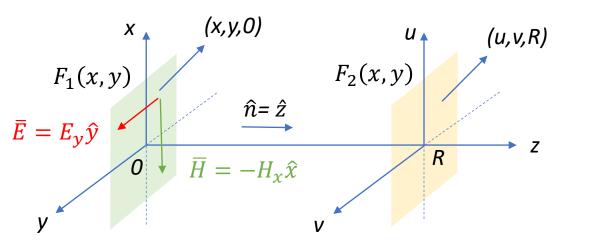
- Transmission region in a LoS (Line-of-sight) environment
 - ✓ Reactive near field region: Energy is stored without radiation.
 - ✓ Fresnel region: Different pairs between Tx antenna elements and Rx antenna elements have different channel characteristics.
 - ✓ Fraunhofer region: The field reaches all receiver antenna elements in the same direction.







Relationship between Tx field and Rx field (Fresnel approximation)



$$\bar{J}(\bar{r}) = \hat{n} \times \bar{H} = \hat{z} \times (-H_{\chi} \hat{x}) = -H_{\chi} \hat{y}$$

$$\overline{M}(\overline{r}) = -\hat{n}x\overline{E} = -\hat{z}x(E_y\hat{y}) = E_y\hat{x}$$

$$F_1(x,y)$$
: Tx field (E or H)

$$F_2(x,y)$$
: Rx field (E or H)

$$\bar{r} = (x, y, 0), \bar{r}' = (u, v, R)$$

 $|\bar{r} - \bar{r}'| = \sqrt{(x - u)^2 + (y - v)^2 + R^2}$

$$F_{2}(u,v) = \frac{j}{\lambda} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F_{1}(x,y) \frac{e^{-jk|\bar{r}-\bar{r}'|}}{|\bar{r}-\bar{r}'|} dx dy$$

$$\approx \frac{je^{-jkR}}{\lambda R} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F_{1}(x,y) \exp\left(-\frac{jk}{2R}(u-x)^{2} - \frac{jk}{2R}(v-y)^{2}\right) dx dy$$

$$= \frac{je^{-jkR}}{\lambda R} e^{-\frac{jk}{2Z}(u^{2}+v^{2})} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} F_{1}(x,y) e^{-\frac{jk}{2R}(x^{2}+y^{2})} e^{\frac{jk}{R}(ux+vy)} dx dy$$

Transformation from signals to fields

$$S_1(x,y)$$
: Tx signal, $S_2(u,v)$: Rx signal
$$F_1(x,y) = S_1(x,y) \ e^{\frac{jk}{2R}(x^2+y^2)}, \qquad F_2(u,v) = S_2(u,v) \ e^{-\frac{jk}{2R}(u^2+v^2)}$$

- Relationship between Tx signal and Rx signal
 - ✓ Tx/Rx signals have a 2-dimensional Fourier transform relationship.

$$\begin{split} S_{2}(u,v) &= \frac{je^{-jkR}}{\lambda R} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S_{1}(x,y) \ e^{j\frac{k}{R}(ux+vy)} dxdy \\ &= je^{-jkR} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S_{1}(x,y) \ e^{j2\pi \left[\left(\frac{u}{\sqrt{\lambda R}} \right) \left(\frac{x}{\sqrt{\lambda R}} \right) + \left(\frac{v}{\sqrt{\lambda R}} \right) \left(\frac{y}{\sqrt{\lambda R}} \right) \right]} \frac{dx}{\sqrt{\lambda R}} \frac{dy}{\sqrt{\lambda R}} \\ S_{1}(x,y) &= -je^{jkR} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S_{2}(u,v) \ e^{-j2\pi \left[\left(\frac{x}{\sqrt{\lambda R}} \right) \left(\frac{u}{\sqrt{\lambda R}} \right) + \left(\frac{y}{\sqrt{\lambda R}} \right) \left(\frac{v}{\sqrt{\lambda R}} \right) \right]} \frac{du}{\sqrt{\lambda R}} \frac{dv}{\sqrt{\lambda R}} \end{split}$$

$$S_1(x, y) \stackrel{\text{2-dim. Fourier transform}}{\longleftrightarrow} S_2(u, v)$$

Fresnel Region Transmission

Two one-dim. Fourier transform

$$\checkmark \text{ If } x' = \frac{x}{\sqrt{\lambda R}}, \ y' = \frac{y}{\sqrt{\lambda R}}, \ u' = \frac{u}{\sqrt{\lambda R}}, v' = \frac{v}{\sqrt{\lambda R}},$$
 then $S_2(u', v') = je^{-jkR} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S_1(x', y') \ e^{j2\pi (u'x' + v'y')} dx' dy'$

If
$$S_1(x', y') = S_{1,H}(x')S_{1,V}(y')$$
, $S_2(u', v') = je^{-jkR}S_{2,H}(u')S_{2,V}(v')$,
then $S_{2,H}(u') = \int_{-\infty}^{\infty} S_{1,H}(x')e^{j2\pi u'x'}dx'$, $S_{2,V}(v') = \int_{-\infty}^{\infty} S_{1,V}(y')e^{j2\pi v'y'}dy'$

Spatial resources

- ✓ Tx array size: $A_1 * B_1$, Rx array size: $A_2 * B_2$, distance: R, wavelength: λ
- ✓ Tx space resource: $0 \le x' \le \frac{A_1}{\sqrt{\lambda R}}$, $0 \le y' \le \frac{B_1}{\sqrt{\lambda R}}$
- ✓ Rx space resource: $0 \le u' \le \frac{A_2}{\sqrt{\lambda R}}$, $0 \le v' \le \frac{B_2}{\sqrt{\lambda R}}$

Fresnel Region Transmission

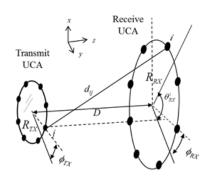
- Time and frequency resource → Fourier transform relationship
 - \checkmark Time resource T, and frequency resource W
 - ✓ Number of information: *T*W*
- Linear array resource → Fourier transform relationship
 - \checkmark Tx array resource $\left(\frac{A_1}{\sqrt{\lambda R}}\right)$, and Rx array resource $\left(\frac{A_2}{\sqrt{\lambda R}}\right)$
 - ✓ Number of modes for linear array: $\left(\frac{A_1}{\sqrt{\lambda R}}\right)\left(\frac{A_2}{\sqrt{\lambda R}}\right) = \frac{A_1A_2}{\lambda R}$
- Planar array resource → 2-dim. Fourier transform relationship
 - ✓ Number of modes for horizontal(vertical) direction array: $\frac{A_1A_2}{\lambda R}$, $\frac{B_1B_2}{\lambda R}$
 - ✓ Number of modes for planar array: $\left(\frac{A_1}{\sqrt{\lambda R}}\right)\left(\frac{B_1}{\sqrt{\lambda R}}\right)\left(\frac{A_2}{\sqrt{\lambda R}}\right)\left(\frac{B_2}{\sqrt{\lambda R}}\right) = \frac{A_1A_2B_1B_2}{(\lambda R)^2}$

(Example)

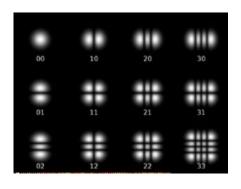
Carrier frequency: 150 GHz, $\lambda=2$ mm, R=3 m, $A_1=A_2=B_1=B_2=20$ cm

Number of modes: $\frac{20cm*20cm*20cm*20cm}{(3m*2mm)^2} = 44$

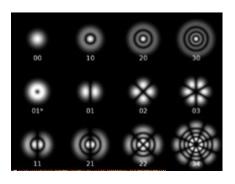
- System design for spatial multimode transmission
 - ✓ Channel environment: LoS environment
 - ✓ In optics, various multi-mode transmission schemes such as OAM, Hermite Gaussian and Laguerre Gaussian modes, have been studied.
 - ✓ In order to apply it to wireless communication environment, it is necessary to develop a transmission scheme that addresses RF impairment problems and supports user mobility.



< OAM mode >



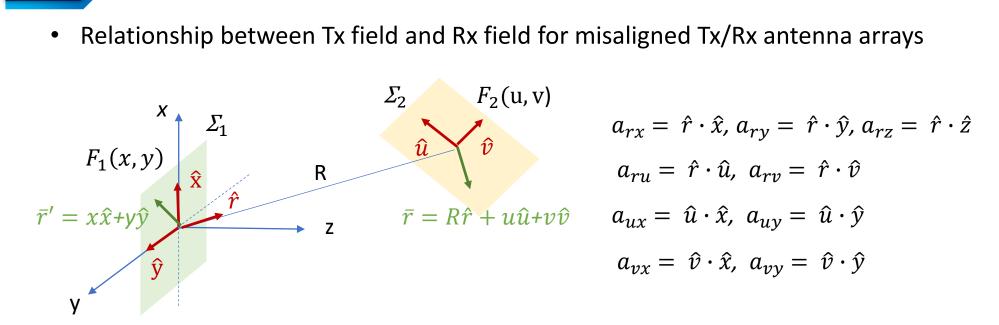
< HG mode >



< LG mode >

- Beamforming for mobility
 - √ 5G beamforming for mobility
 - : Far-field region beamforming
 - : Polarized streams can be transmitted in each beam
 - ✓ 6G beamforming for mobility
 - : Fresnel region beamforming
 - : Multiple modes can be transmitted simultaneously in each beam
- Beamforming for misalignment
 - ✓ When Tx antenna and Rx antenna are not aligned, is it possible to obtain Fourier transform relationship between Tx signal and Rx signal?
 - ✓ Yes, beamforming can make Fourier transform relationship betwen Tx and Rx signals.

Relationship between Tx field and Rx field for misaligned Tx/Rx antenna arrays



$$\bar{r}' = x\hat{x} + y\hat{y}, (x,y) \in \Sigma_{1}, \ \bar{r} = R\hat{r} + u\hat{u} + v\hat{v}, (u,v) \in \Sigma_{2}$$

$$F_{2}(u,v) = \frac{j}{\lambda} \iint_{\Sigma_{1}} F_{1}(x,y) \frac{e^{-jk|\bar{r}-\bar{r}'|}}{|\bar{r}-\bar{r}'|} a_{rz} dx dy$$

$$\approx \frac{je^{-jkz}}{\lambda R} e^{-jk(ua_{ru}+va_{rv})} e^{-\frac{jk}{2R}(u^{2}+v^{2})}$$

$$\iint_{\Sigma_{1}} F_{1}(x,y) e^{jk(xa_{rx}+ya_{ry})} e^{-\frac{jk}{2R}(x^{2}+y^{2})} e^{j\frac{k}{R}(uxa_{ux}+uya_{uy}+vxa_{vx}+vya_{vy})} a_{rz} dx dy$$

Tx/Rx beamforming for mobile users

$$S_1(x,y)$$
: Tx signal $S_2(x,y)$: Rx signal

(1) Tx beamforming

$$F_1(x,y) = S_1(x,y)e^{-jk(xa_{rx}+ya_{ry})}e^{j\frac{k}{2R}(x^2+y^2)}$$
Tx beamforming

(2) Rx beamforming

$$S_2(u,v) = F_2(u,v)e^{jk(ua_{ru}+va_{rv})}e^{-j\frac{k}{2R}(u^2+v^2)}$$
Rx beamforming

(3) Relationship between Tx signal and Rx signal

$$S_{2}(u,v) = \frac{je^{-jkR}}{\lambda R} \iint_{\Sigma_{1}} S_{1}(x,y) e^{j\frac{k}{R}(uxa_{ux} + uya_{uy} + vxa_{vx} + vya_{vy})} a_{rz} dx dy$$

Coordinate transformation

$$\alpha = xa_{ux} + ya_{uy}$$

$$\beta = xa_{vx} + ya_{vy}$$

$$uxa_{ux} + uya_{uy} + vxa_{vx} + vya_{vy} = u\alpha + v\beta$$

$$\begin{pmatrix} \alpha \\ \beta \end{pmatrix} = T \begin{pmatrix} x \\ y \end{pmatrix}, \quad T = \begin{pmatrix} a_{ux} & a_{uy} \\ a_{vx} & a_{vy} \end{pmatrix}$$

$$Area: A_1 B_1$$

$$Area: |D|A_1 B_1$$

$$\begin{pmatrix} x \\ y \end{pmatrix} = T^{-1} \begin{pmatrix} \alpha \\ \beta \end{pmatrix}, \quad T^{-1} = \frac{1}{D} \begin{pmatrix} a_{vx} & -a_{uy} \\ -a_{vx} & a_{uy} \end{pmatrix}, \quad D = \begin{vmatrix} a_{ux} & a_{uy} \\ a_{vx} & a_{vy} \end{vmatrix} = a_{ux} a_{vy} - a_{uy} a_{vx}, \quad |D| \le 1$$

$$Q_1(\alpha, \beta) = S_1(x, y) = S_1(T^{-1}(\alpha, \beta)) = S_1 \left(\frac{1}{D} (a_{vy}\alpha - a_{uy}\beta), \frac{1}{D} (-a_{vx}\alpha + a_{ux}\beta)\right)$$

$$S_2(u, v) = \frac{je^{-jkR}}{\lambda R} \frac{a_{rz}}{|D|} \iint_{A_1} Q_1(\alpha, \beta) e^{j\frac{k}{R}(u\alpha + v\beta)} d\alpha d\beta$$

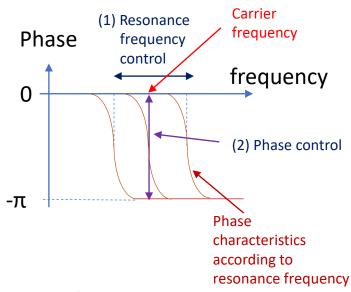
 $Q_1(\alpha, \beta) \stackrel{\text{2-dim. Fourier transform}}{\longleftrightarrow} S_2(u, v)$

- Number of modes (rank)
 - ✓ Transmitter antenna array size: $A_1 * B_1$
 - ✓ Receiver antenna array size: A_2*B_2
 - \checkmark Number of modes: $\frac{A_1B_1A_2B_2}{(\lambda R)^2}|D|$, $\left(D = a_{ux} a_{vy} a_{uy} a_{vx}\right)$
- Effect of non-pararell antenna arrays
 - ✓ Capacity may decrease if tx antenna array is not parallel to rx antenna array.
 - ✓ If Tx/Rx antenna arrays are parallel to each other, then |D| = 1, and the number of modes and capacity are maximized.

Reconfigurable Intelligent Surface

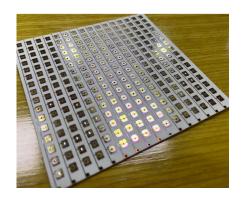
- Reconfigurable intelligent surface
 - ✓ Can overcome the shadowing problem in an NLoS environment.
 - ✓ Can be utilized for beamforming for mobile users.
 - ✓ Reflection type, transmittance type
- What should be considered about RIS?
 - ✓ RIS can be used in beamforming.
 - ✓ You should be able to change phases easily.
 - ✓ Controlling the amplitude is not that important.
- Principle of RIS

✓ RIS can change the phase characteristics at the carrier frequency by controlling the resonance frequency.

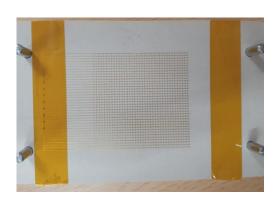


Reconfigurable Intelligent Surface

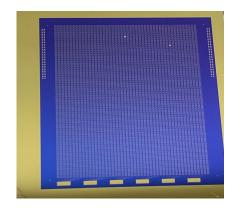
- How to control resonance frequency
 - ✓ Varactor diode: control capacitance (Upper-mid band, 24 GHz)
 - ✓ Graphene: control chemical potential (Sub-THz, 150 GHz, 300 GHz).
 - ✓ Liquid crystal: control permittivity (Sub-THz, 150 GHz, 300 GHz)



< Varactor based RIS >



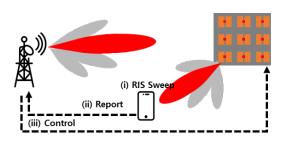
< LC based RIS >



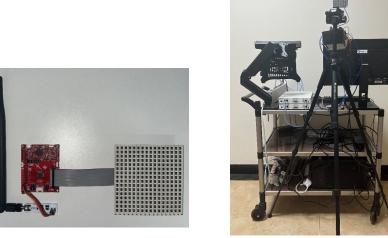
< Graphene based RIS >

Reconfigurable Intelligent Surface

RIS implementation in 6G upper-mid band (varactor diode)



< Concept of RIS beam control>



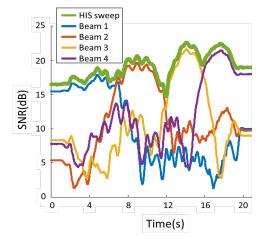
< RIS and RIS controller >



< Tx system (Rx system) >



< Real-time RIS operation in indoor environment >



< Measurement results >

- 1) Beam 1~4
- metasurface beamforming pattern 1~4
- 2) HIS sweep
- beamforming pattern giving the best SNR value

5 Conclusion

Multi-mode transmission for 6G 1 Tbps capacity

- ✓ Time and space resources should be utilized effectively.
- ✓ In sub-THz band, the number of modes and capacity are determined by antenna array size and transmission distance.
- ✓ Through transmitting multiple modes per each beam, we can achieve
 1 Tbps capacity, which is one of the goals of 6G wireless communication.

Beamforming for mobility

- ✓ Beamforming is also required to serve mobile users.
- ✓ There is a need to develop a low complexity method for multi-mode transmission and beamforming.

RIS for 6G solution

- ✓ RIS allows you to overcome the shadowing problem.
- ✓ RIS can be effectively used in low complexity beamforming solutions.

